

WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

### GPIHI8ICDF68

#### GaN Power IC in DFN6x8 Package

#### Preliminary Datasheet version: 1.2

### <u>Features</u>

| BV <sub>dss</sub> | R <sub>dson</sub> | Vbus |  |
|-------------------|-------------------|------|--|
| 900V              | 170 mΩ            | 650V |  |

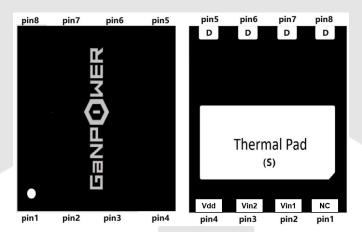
- Edge-triggered high-side power IC
- Small transformer isolation
- Low Rds and high dv/dt capability
- Extremely low input capacitance
- Fast switching and Low Profile

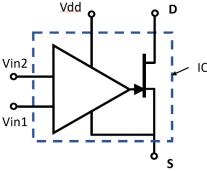
## **Applications**

- High-side switch in switching power applications
- Power adapters and power delivery chargers
- Start-up procedure: Please set Vdd to be a normal operation voltage (e.g., 6.5V) before turning on the high voltage power supply or applying high voltage to the drain. Vdd is the power supply for the internal gate driver in our GaN Power IC. Only when a normal operation voltage (e.g., 6.5V) is applied to Vdd, will the internal driver and GaN HEMT work properly.
- Application configuration: Edge triggered Vin1 and Vin2 pulses control the Vgs on/off. Device turn-on is achieved when Vin2 is edge-triggered and device turn-off is achieved when Vin1 is edge-triggered.

### **Description**

These devices are power IC based on 650V Power GaN HEMTs using proprietary (US patent issued) E-mode GaN on silicon technology. The gate driver is integrated with the main power transistor resulting in fast switching, high system power density and low cost. Edge triggering narrow pulse is used to control device turn-on/off. This results in high noise immunity and a small and inexpensive transformer for isolation and level shifting for the







WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

high-side switch in a half bridge application.

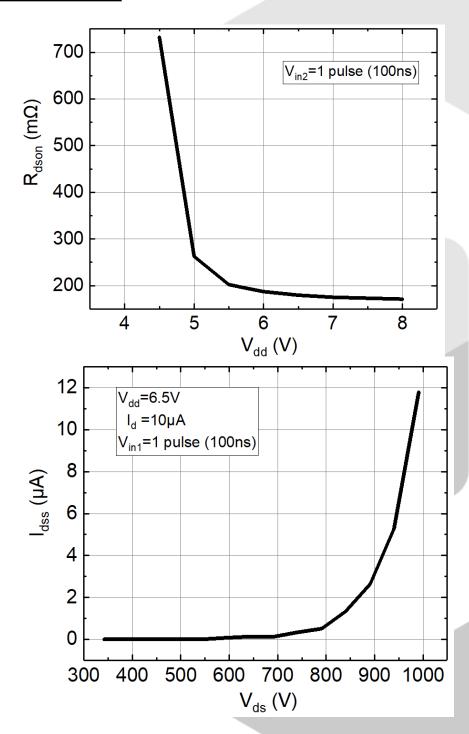
# **Device Characteristics**

| Basic Parameters      |                    |  |   | Test data |         |     |      |
|-----------------------|--------------------|--|---|-----------|---------|-----|------|
|                       | Parameters         |  | Conditions  | Min       | Typical | Max | Unit |
| 1                     | $BV_dss$           | Drain-Source breakdown voltage                           | $V_{dd} = 6.5V$ $I_d = 10 \mu A$ $V_{in1} = 1 \text{ pulse}$ $(100-300 \text{ ns})$ |           | 900     |     | V    |
| 2                     | l <sub>dss</sub>   | Zero gate voltage drain current,<br>$T_c = 25$ °C        | $V_{dd} = 6.5V$<br>$V_{ds} = 900V$<br>$V_{in1} = 1$ pulse<br>(100-300ns)            |           | 2.6     |     | μΑ   |
| 3                     | $R_{dson}$         | Static drain-source on resistance, T <sub>c</sub> = 25°C | $V_{dd} = 6.5V$<br>$V_{in2} = 1$ pulse<br>(100-300ns)                               |           | 170     | 180 | mΩ   |
| 4                     | $V_{dd}$           | Drive supply voltage                                     |   | 5         | 6.5     | 8   | V    |
| 5                     | l <sub>dd</sub>    | Driver supply current                                    | V <sub>dd</sub> = 6.5V  |           | 3       | 4   | mA   |
| 6                     | $V_{in1}$          | Turn-off narrow triggering pulse                         | Pulse width<br>100-300ns  | 2.5       | 5       | 8   | V    |
| 7                     | V <sub>in2</sub>   | Turn-on narrow triggering pulse                          | Pulse width<br>100-300ns  | 2.5       | 5       | 8   | V    |
| Switching Performance |                    |  |   | Test data |         |     |      |
|                       | Parameters         |  | Conditions  | Min       | Typical | Max | Unit |
| 1                     | t <sub>d(on)</sub> | Turn-on delay time                                       | V <sub>ds</sub> =400V   |           | 11      |     | ns   |
| 2                     | t <sub>r</sub>     | Rise time  | I <sub>d</sub> =1A  |           | 29      |     | ns   |
| 3                     | $t_{d(off)}$       | Turn-off delay time                                      | V <sub>in1/2</sub> =5V  |           | 8       |     | ns   |
| 4                     | t <sub>f</sub>     | Fall time  | V <sub>dd</sub> =6.5V   |           | 34      |     | ns   |



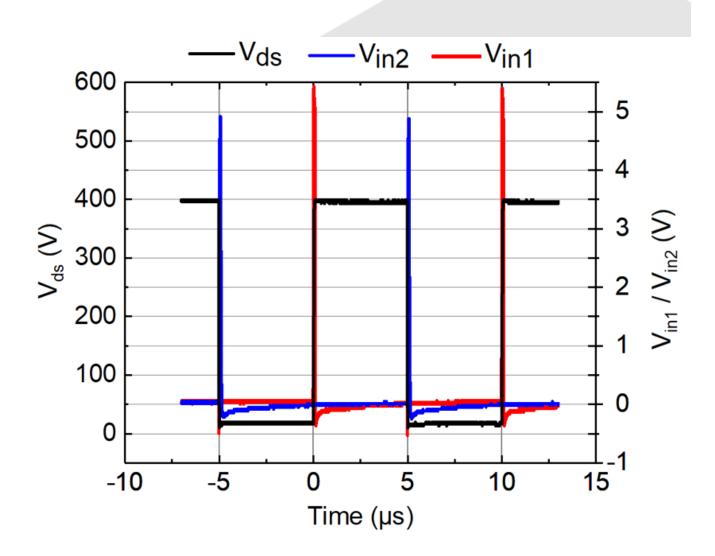
WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

# **Electrical Performance**





WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

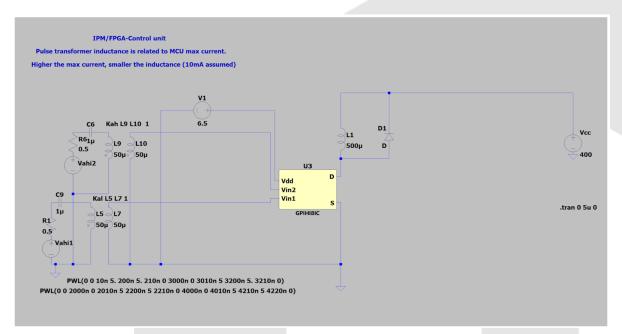


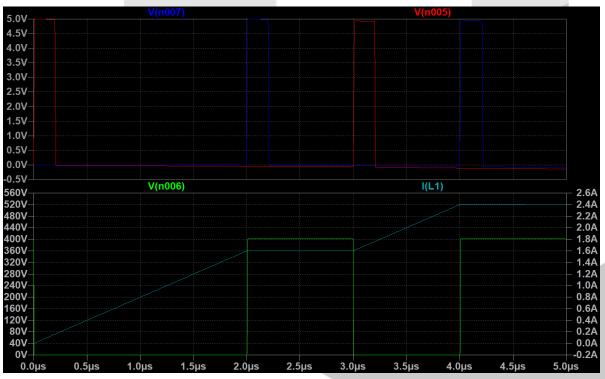
DPT test:  $V_{bus}$  = 400V (100kHz),  $V_{in1}/V_{in2}$  pulse width = 100ns, R-load = 500 $\Omega$ 



WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

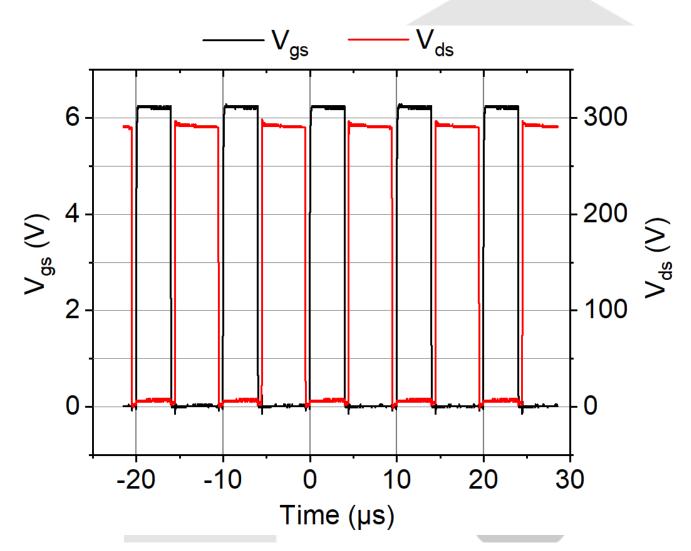
## LTSpice Simulation (DPT with L-load)







WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

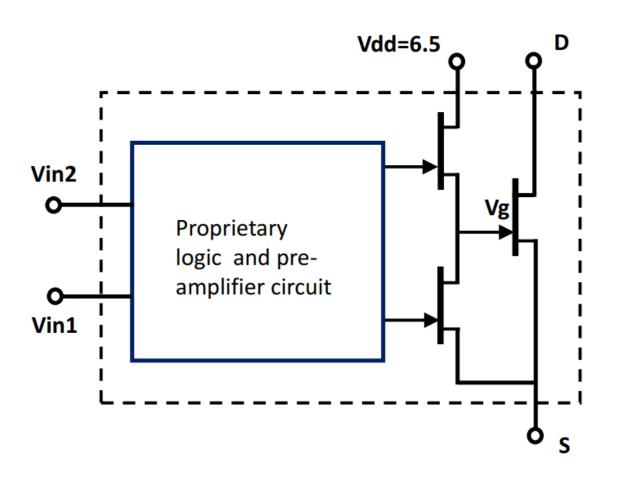


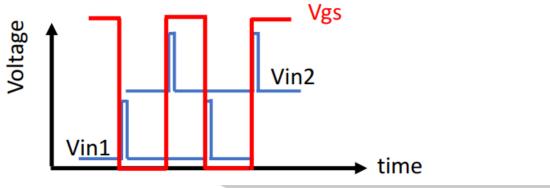
Half-bridge buck at  $V_{bus}$  = 300V (100kHz), R-load = 160 $\Omega$ 



WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

# **Internal Schematic and waveforms**

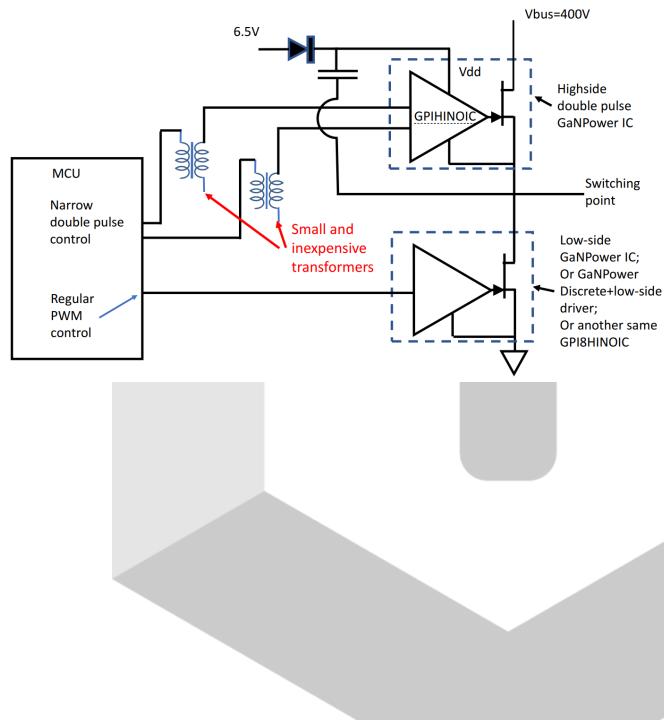






WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

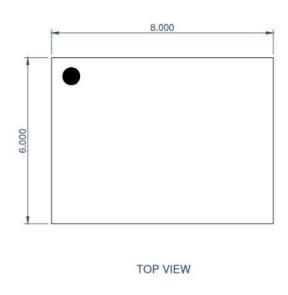
### Typical Application Circuit (Conceptual)

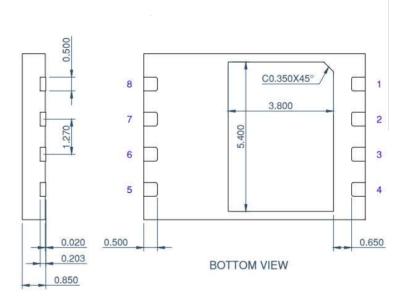




WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

# **Package Information**





PKG nom. thickness : 0.85mm (Y type) LF THICKNESS : 0.203±0.008 THK





WWW. IGANPOWER.COM 230 -3410 LOUGHEED HWY VANCOUVER, BC, V5M 2A4 CANADA

# **GaN HEMT Frequently Asked Questions**

| 1 | Q: Can we do pin to pin switch for silicon MOSFET or IGBT?                                      |
|---|---|
|   | A: The short answer is no. GaN HEMT power devices are far superior than the best silicon        |
|   | devices such as super junction MOSFETs. However, due to different requirements of gate          |
|   | driving voltage and extremely high dv/dt slew rate, special drivers and optimized PCB layouts   |
|   | are recommended to minimize the impact from circuit parasitics. Some packaging forms such       |
|   | as GaNPower's DFN packaged devices offer both sense and force for the source terminal.          |
|   | Also, for traditional TO220 packages, please be advised that the pins are arranged as Gate –    |
|   | Source -Drain, and the thermal pad is connected to the source instead of drain.                 |
| 2 | Q: Are GaN power devices reliable?  |
|   | A: GaN power HEMTs have been tested by GaNPower and many other vendors, users and               |
|   | testing facilities to be as reliable (if not better than) silicon counterparts.                 |
| 3 | Q: How do GaN power devices compare with SiC?   |
|   | A: Currently GaN power HEMT devices are most suitable for low to medium voltage (≤1200V)        |
|   | and power (<50KW) applications.   |
| 4 | Q: Do we need to parallel an FRD for applications such as inverters?                            |
|   | A: GaN devices are different from silicon MOSFET or IGBT in that they have no inherent PN       |
|   | junction diodes that cause reverse recovery issue. User do not need to parallel an FRD for the  |
|   | purpose of suppressing the body diode reverse recovery effect, since GaN HEMT can operate       |
|   | in both first and third quadrants. However, care should be taken for the dead time power loss   |
|   | since the Vsd voltage of GaN HEMT is usually close to 2V. This is especially true when a        |
|   | negative gate voltage is applied.   |
| 5 | Q: Can we parallel GaN HEMT devices?  |
|   | A: Yes, GaN HEMT is ideal for paralleling, due to the positive temperature coefficient of Rdson |
|   | and slightly positive temperature coefficient of threshold voltage.                             |